



21ème Colloque International & Exposition sur la Compatibilité Électromagnétique



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MICROSTRIP STRUCTURE RESONANCE NGD-EQUALIZATION

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Outline

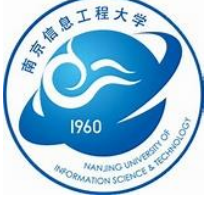
A/ State of the Art (SoA) on negative group delay (NGD) circuits

B/ NGD ideal specifications and design method

C/ Principle of NGD equalization

D/ Discussion on Proof-of-concept (PoC) result showing resonance reduction

E/ Conclusion



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A/ SoA on negative group delay (NGD) circuits

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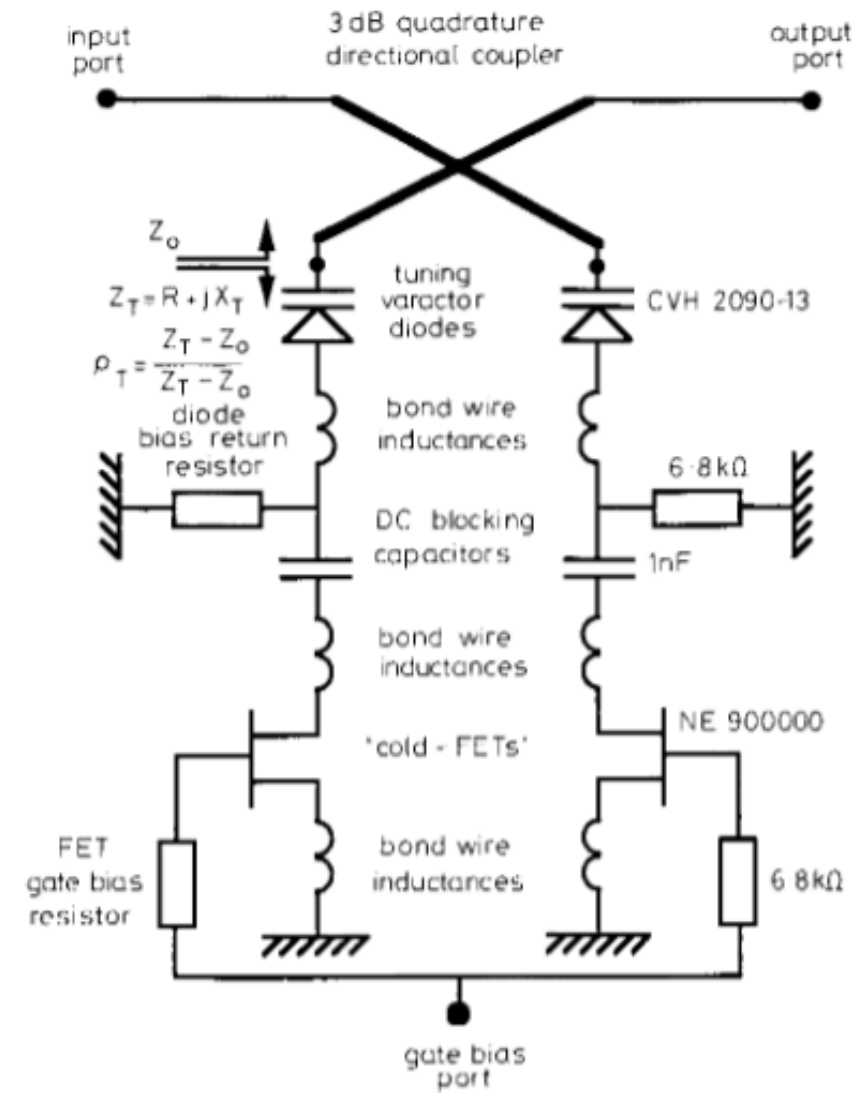
E/ Conclusion



H. Du, F. Wan, M. Guerin, F. Haddad, W. Rahajandraibe, G. Fontagalland & B. Ravelo, "Microstrip structure resonance NGD-equalization," Proc. of 21ème Colloque International & Exposition sur la CEM (CEM 2023), 13-15 June 2023, Toulouse, France, pp. 1-5

A/ SoA on NGD circuits

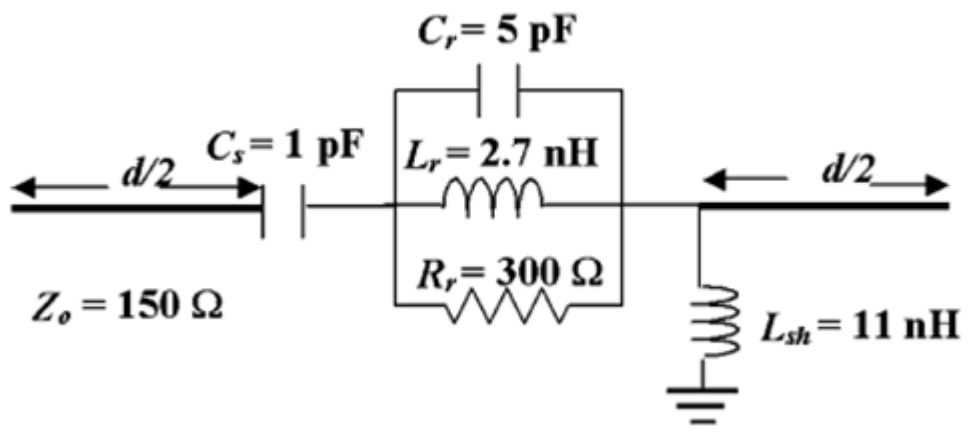
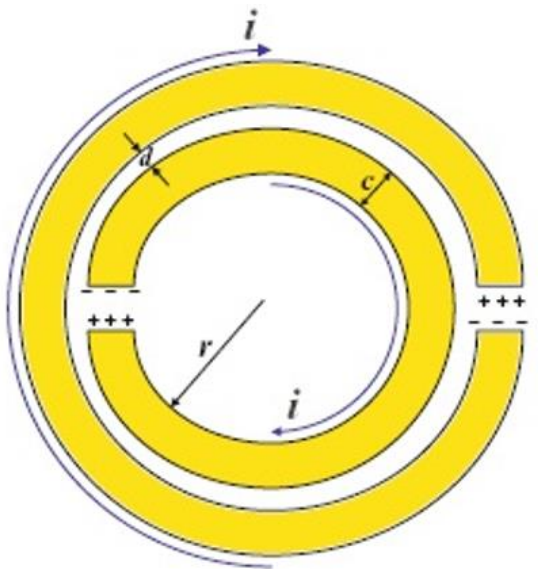
- ❑ In the early 1990s, the NGD effect was demonstrated in electronics engineering ...
- ❑ Theoretical and experimental investigations in the field of RF and microwave engineering confirmed that certain passive and active circuit topologies are susceptible to generate the NGD phenomenon^{1,2}
- ❑ Based on the GD analytical definition, this counterintuitive physical phenomenon occurs when the linear circuit or media structure differential phase presents a positive slope in function of the frequency^{1,2}



¹ S. Lucyszyn, I. D. Robertson and A. H. Aghvami, "Negative Group Delay Synthesiser," *Electron. Lett.*, Vol. 29, 1993, pp. 798-800

² S. Lucyszyn and I. D. Robertson, "Analog Reflection Topology Building Blocks for Adaptive Microwave Signal Processing Applications," *IEEE Trans. MTT*, Vol. MTT-43, No. 3, Mar. 1995, pp. 601-611

A/ SoA on NGD circuits

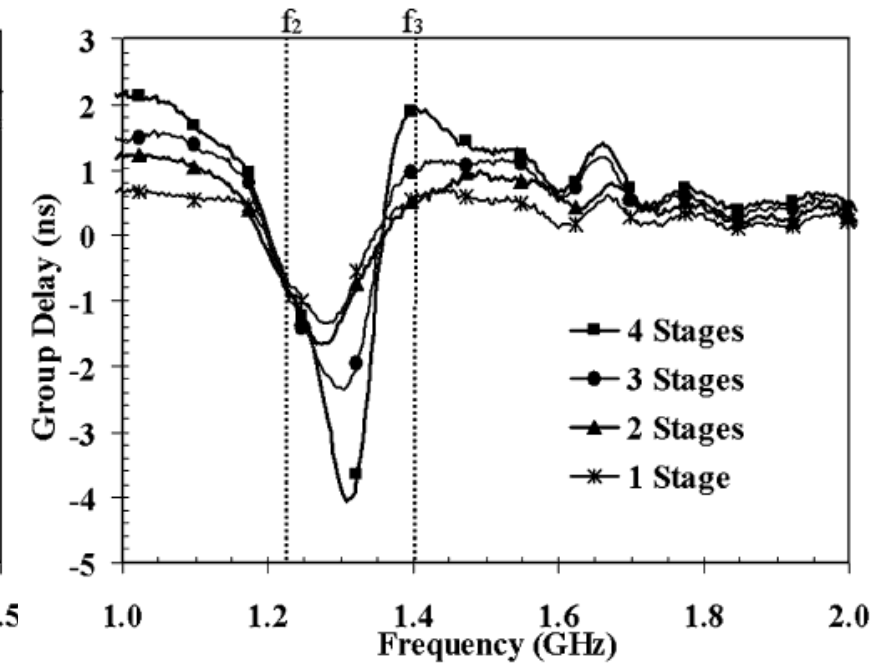
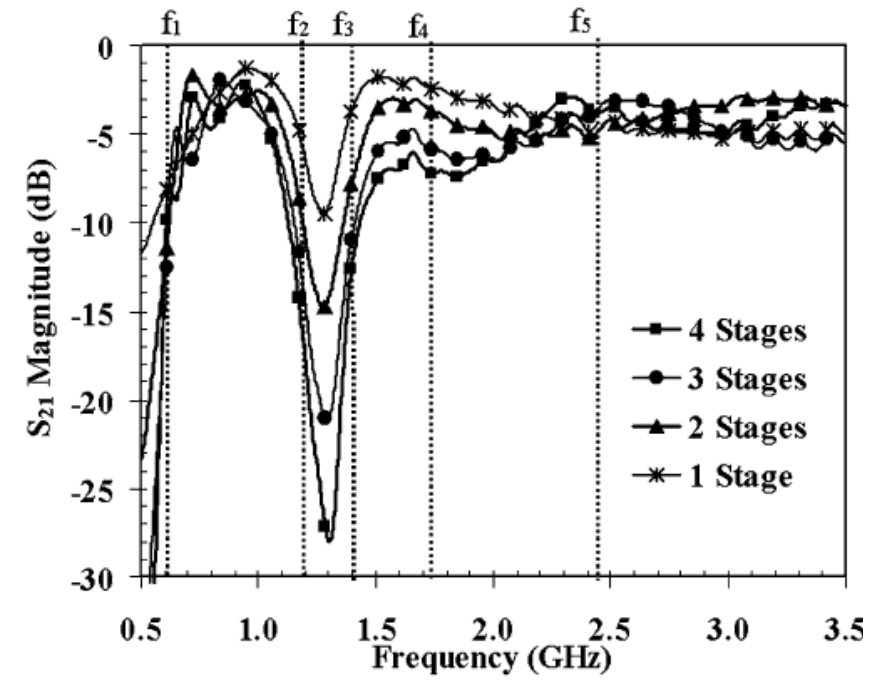


- ❑ In 2000s, more interests on NGD study was developed by using the TL and passive/active RF/microwave circuit theories
- ❑ The NGD electrical equivalent circuit^{15,16,17} was established in function of the split ring resonator (SRR) physical and geometrical parameters by considering the transmittance
- ❑ The NGD distributed equivalent circuit^{15,16,17} was established from physical dimension reduction 3-D-to-2-D and 2-D-to-1-D
- ❑ The equivalent NGD circuit constituted by classical R, L and C component elements was obtained from 1-D-to-0-D transpositions^{15,16,17}

¹⁵ O. F. Siddiqui, et al, *IEEE T-AP*, Vol. 51, No. 10, pp. 2619-2625, Oct. 2003
¹⁶ G. V. Eleftheriades, et al, *IEEE MWCL*, Vol. 13, No. 2, Feb. 2003
¹⁷ O. F. Siddiqui, et al, *IEEE T-MTT*, Vol. 52, No. 5, May, 2004

A/ SoA on NGD circuits

- Theoretical and experimental studies confirm the NGD effect at RF and microwave frequencies
- But, the periodical SRR-based structures operate with more than 20 dB attenuation in order to generate significant NGD values
- Therefore, research works were made on the development of low attenuation loss NGD circuits



¹⁵ O. F. Siddiqui, et al, IEEE T-AP, Vol. 51, No. 10, pp. 2619-2625, Oct. 2003

¹⁶ G. V. Eleftheriades, et al, "IEEE MWCL, Vol. 13, No. 2, Feb. 2003

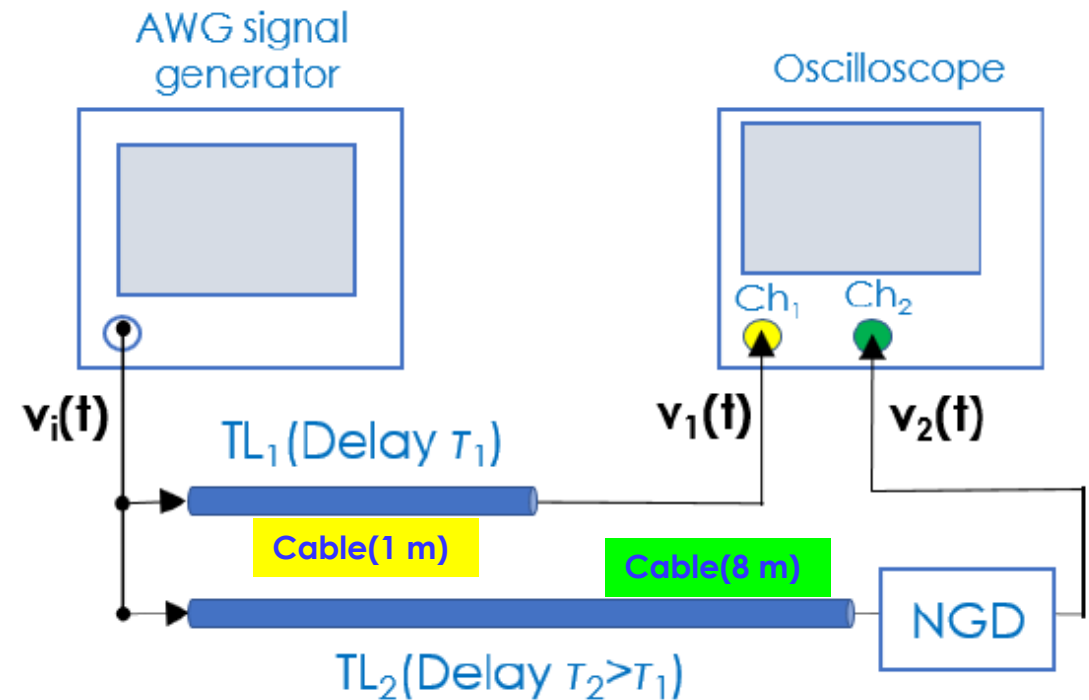
¹⁷ O. F. Siddiqui, et al, IEEE T-MTT, Vol. 52, No. 5, May, 2004



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A/ SoA on NGD circuits

- ❑ The meaning and interpretation of NGD effect remain an open question to SI/EMC design and test engineers
- ❑ To highlight the meaning of negative time ($t < 0$), some experimentations^{1,2,3} were experimented at NUIST in early 2020s
- ❑ ... Some demos of $t < 0$ for reducing or cancelling out the **propagation delay** (**cable(8 m)+NGD**) < **Delay(cable(1 m))**



¹ F. Wan, T. Gu, B. Ravelo, B. Li, J. Cheng, Q. Yuan and J. Ge, "NGD Theory of a Four-Port RC-Network Feedback Operational Amplifier," IEEE Access, Vol. 7, No. 1, Dec. 2019

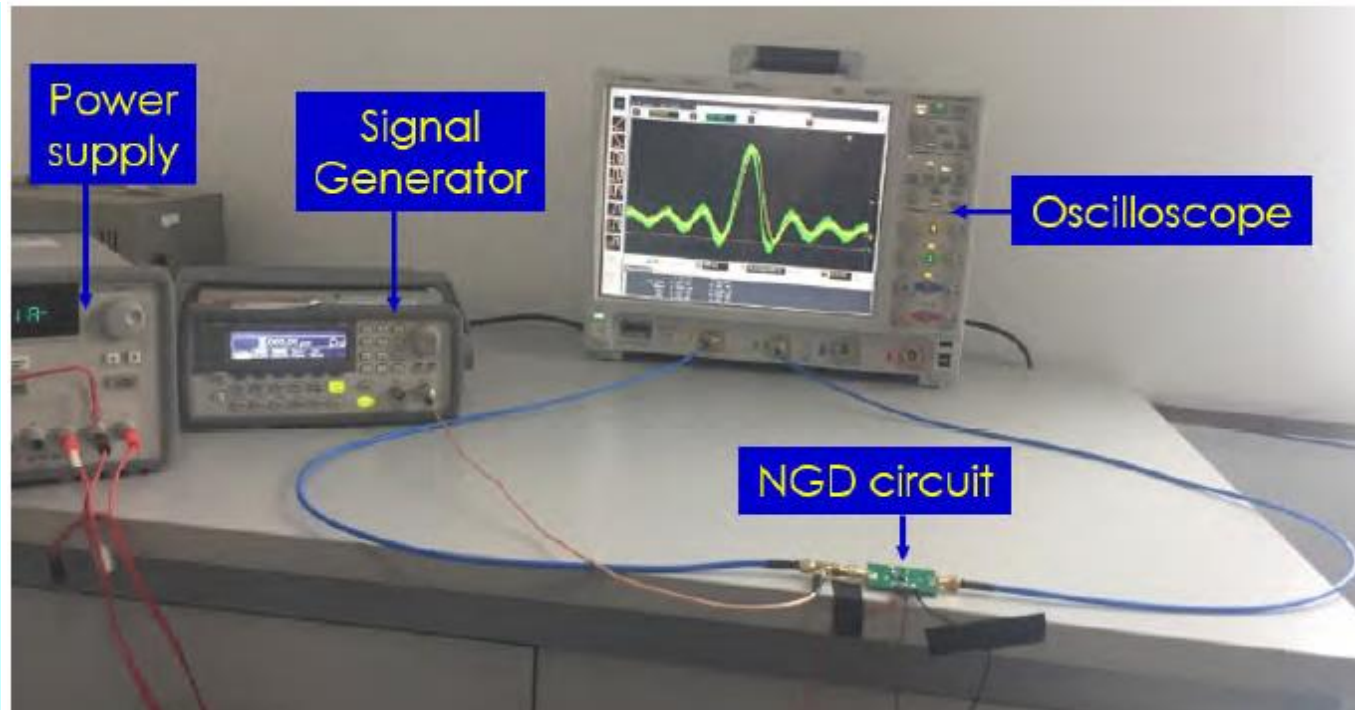
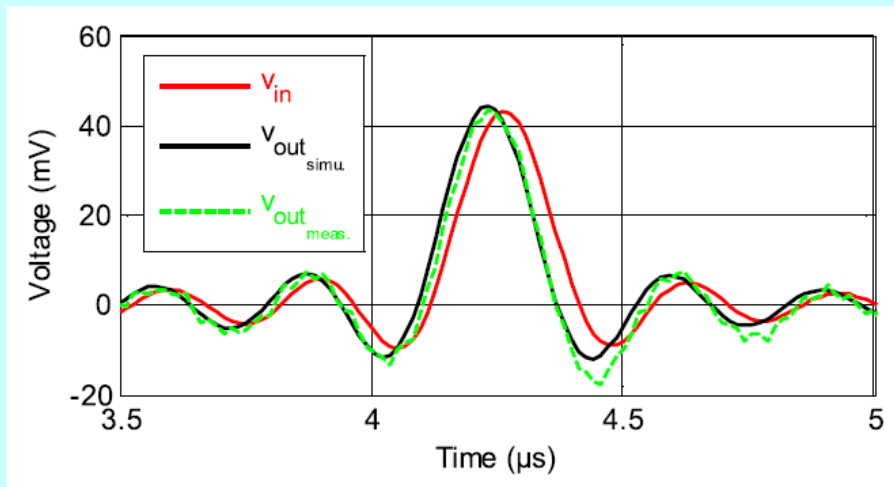
² F. Wan, X. Miao, B. Ravelo, Q. Yuan, J. Cheng, Q. Ji, and J. Ge, "Design of Multi-Scale NGD Circuit for Sensors Signal Time-Delay Cancellation," IEEE Sensors Journal, Vol. 19, No. 19, Oct. 2019

³ F. Wan, J. Wang, B. Ravelo, J. Ge, and B. Li, "Time-Domain Experimentation of NGD Active RC-Network Cell", IEEE Trans. CAS II: Express Briefs, Vol. 66, No. 4, Apr. 2019

A/ SoA on NGD circuits

Recent wonderful NGD experimentations^{1,2,3}

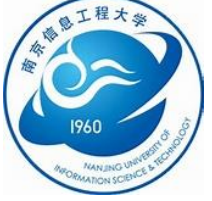
- Observation of $t < 0$
- Delay(cable(8 m)+NGD) < Delay(cable(1 m))**



¹ F. Wan, T. Gu, B. Ravelo, B. Li, J. Cheng, Q. Yuan & J. Ge, "Negative Group Delay Theory of a Four-Port RC-Network Feedback Operational Amplifier," *IEEE Access*, Vol. 7, No. 1, Dec. 2019

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B/ NGD ideal specifications and design method

C/ Principle of NGD equalization

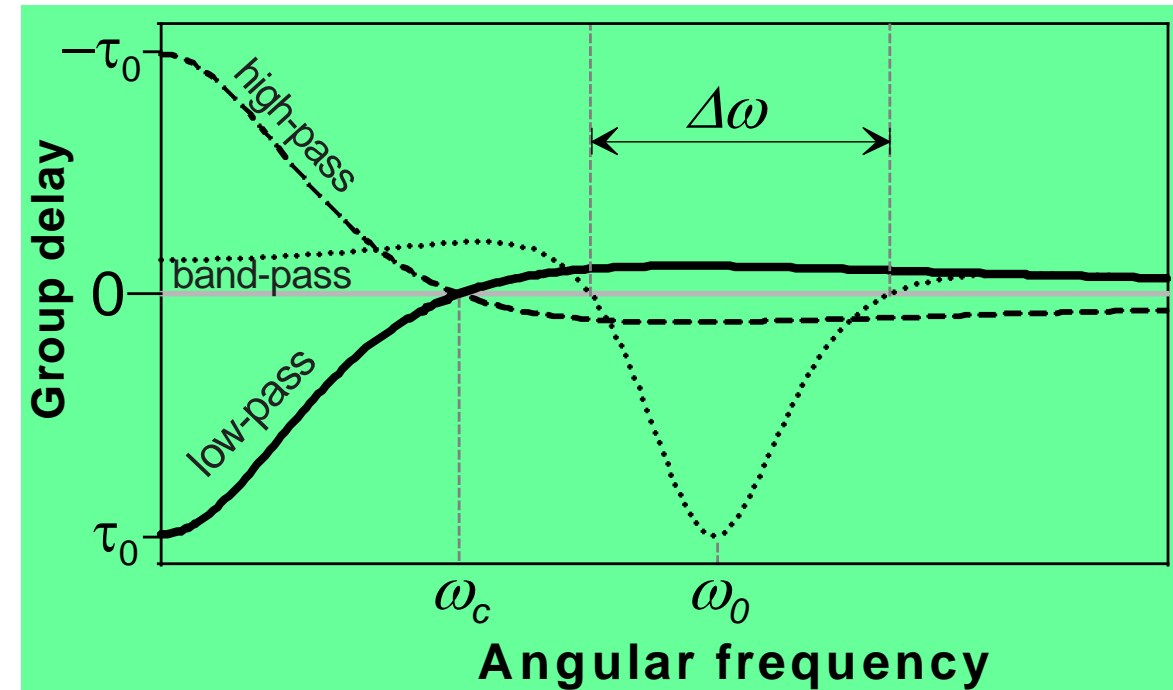
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- ❑ An NGD design is necessary to democratize further the topic to all electronic design, fabrication, test and commercial engineers
- ❑ Elementary topologies of NGD cells were identified in function of the GD diagram and the NGD frequency band positioning
- ❑ By the analogy with the filter theory, the classes of NGD functions were initiated:
 - 👍 Low-pass (LP) NGD function
 - 👍 High-pass (HP) NGD function
 - 👍 **Bandpass (BP) NGD function**
 - 👍 Stop-band (SB) NGD function
 - 👍 All-pass (AP) NGD function



¹ B. Ravelo, "Methodology of elementary negative group delay active topologies identification," *IET Circuits Devices Syst.*, May 2013

² B. Ravelo, "Similitude between the NGD function and filter gain behaviours," *Int. J. Circ. Theor. Appl.*, Oct. 2014

B. Ravelo, "On the low-pass, high-pass, bandpass and stop-band NGD RF passive circuits," *URSI Radio Science Bulletin*, Vol. 2017, No. 363, Dec. 2017, pp. 10-27

Characteristics	Normal Filter	NGD Function
Basic specifications	Transfer function gain	Transfer function group delay
Cutoff frequencies ω_c	Root of the equation $ S_{21}(j\omega_c) = S_{21}(j\omega) _{\max} / \sqrt{2}$	Root of the equation $\tau(\omega_c) = 0$
Bandwidth	$ S_{21}(j\omega_c) \geq S_{21}(j\omega) _{\max} / \sqrt{2}$	$\tau(\omega) \leq 0$
Low-pass with bandwidth defined by $\omega \leq \omega_c$	In the bandwidth, we have $ S_{21}(j\omega_c) \geq S_{21}(j\omega) _{\max} / \sqrt{2}$	In the bandwidth, we have $\tau(\omega) \leq 0$ and $ S_{21}(j\omega) $ should be as flat as possible.
High-pass with bandwidth defined by $\omega \geq \omega_c$		
Bandpass with bandwidth defined by $\omega_{c1} \leq \omega \leq \omega_{c2}$		
Stop-band with bandwidth defined by $\omega \leq \omega_{c1}$ and $\omega \geq \omega_{c2}$		

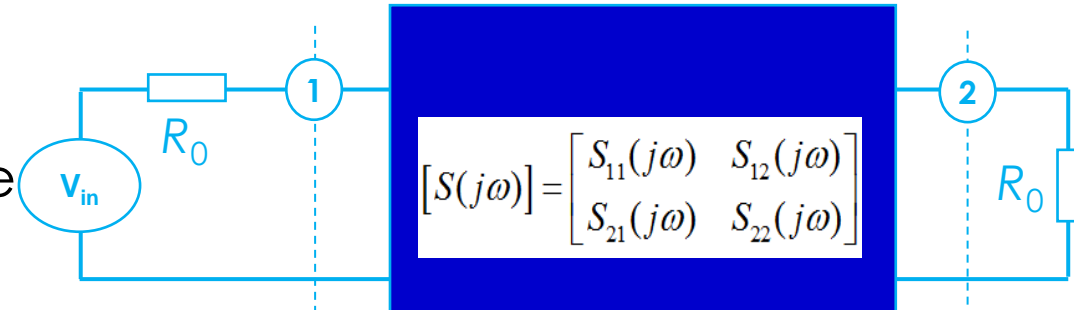
B/ NGD ideal specifications & design method

❑ The NGD specifications are defined from magnitude and GD diagrams

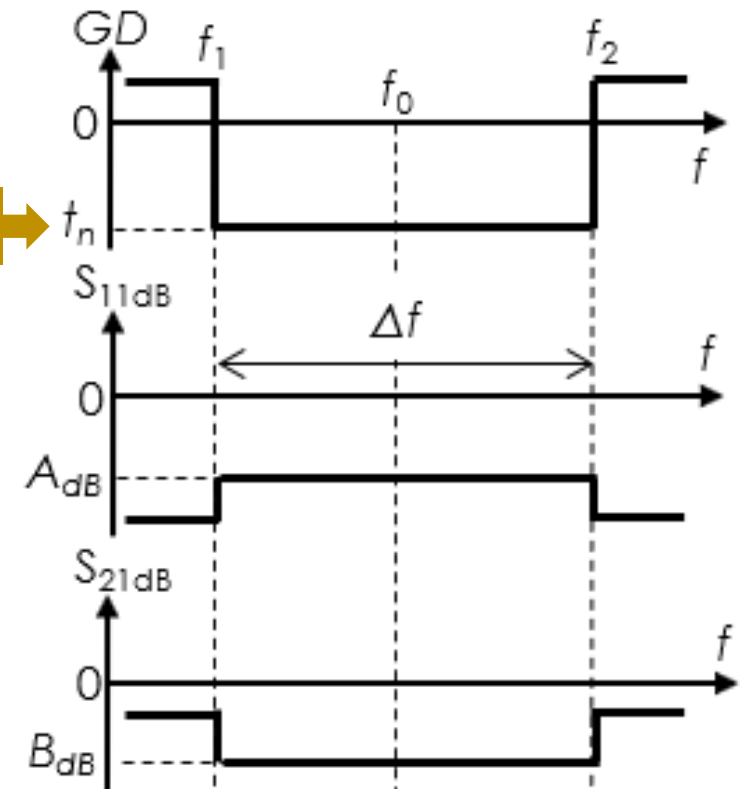
❑ BP-NGD circuit specifications:

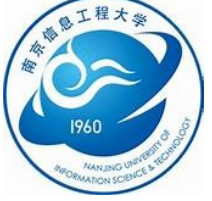
- ✓ NGD center frequency: f_0
- ✓ NGD value: $t_n = \text{GD}(f_0) < 0$
- ✓ Insertion loss: $|s_{21}(f_0)|$
- ✓ Reflection losses: $|s_{11}(f_0)|, |s_{22}(f_0)|$
- ✓ NGD bandwidth: $\Delta f = f_2 - f_1$

❑ BP-NGD NGD figure of merit (FoM) for passive circuits integrating these different parameters can be defined by: $\text{FoM}_{\text{NGD}} = t_n \cdot \Delta f \cdot \sqrt{(|s_{21}(f_0)| / |s_{11}(f_0)|)}$



Negative 😊 →





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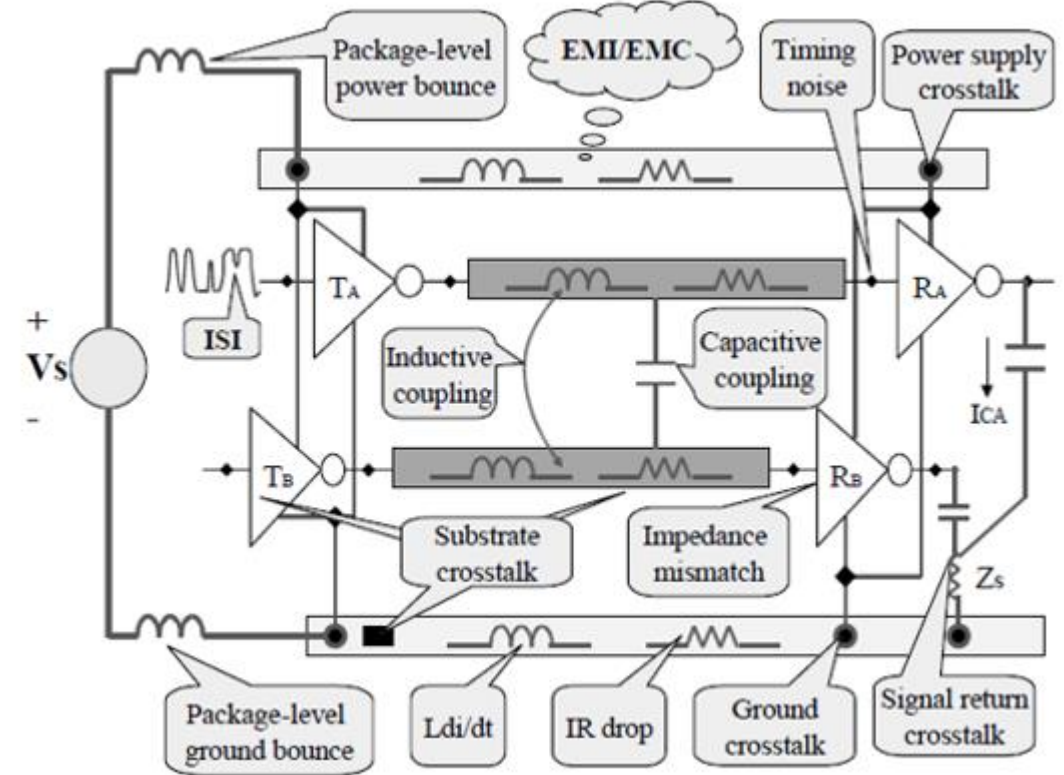
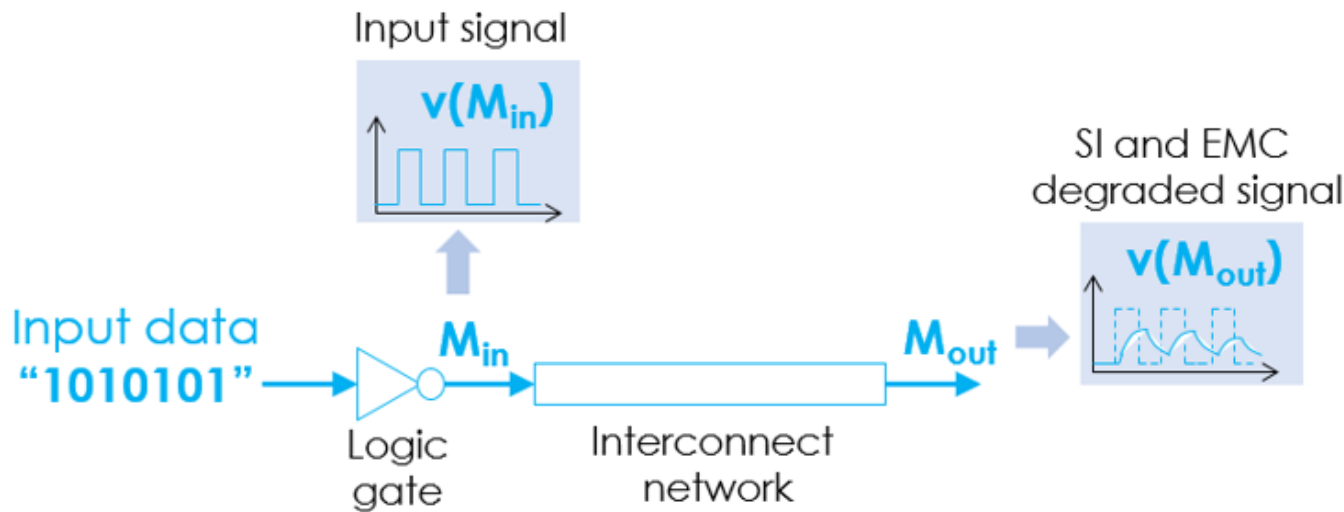


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C/ Principle of NGD equalization

❑ How to minimize or cancel out the undesired EMC/EMI, SI and PI¹ effects in the high density as in the mixed circuits?

❑ In term of SI, we can underline that propagation delay and distortion may induce undesirable ISI and they limit the HDI circuit performance as the speed of operation data ($f_{max} < 1/\text{delay}$)



¹ L.-R. Zheng and H. Tenhunen, "Wires as interconnects", chap. 2, interconnect centric book, 2003

Characterization of EMC and EMI perturbation VTF which causes the signal distortion

- ❑ The parasitic or perturbation is modelled by the VTF $T_p(s)$
- ❑ The input $v_{in}(t)$ is changed into output $v_p(t)$
- ❑ The corresponding VTF can be determined by $T_p(s) = V_p(s) / V_{in}(s)$



B. Ravelo, et al., "New Technique of Inter-Chip Interconnect Effects Equalization with NGD Active Circuits," VLSI, Chap. 20, Intech Book, Feb. 2010, pp. 409-434

B. Ravelo, et al., "Equalization of Interconnect Propagation Delay with NGD Active Circuits," 11th IEEE Workshop on SPI, Genova, Italy, 13-16 May 2007, pp. 15-18

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B. Ravelo, et al., "Experimental Validation of the RC-Interconnect Effect Equalization with Negative Group Delay Active Circuit in Planar Hybrid Technology," 13th IEEE Workshop on SPI, Strasbourg, France, 12-15 May 2009, pp. 1-4

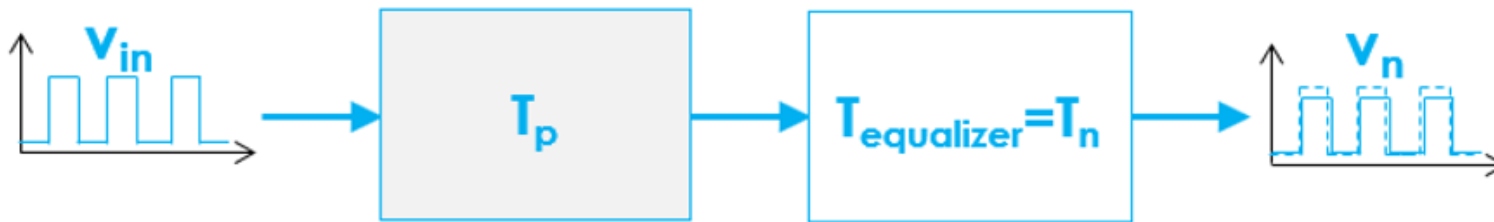
B. Ravelo & Y. Liu, "Microwave/Digital Signal Correction with Integrable NGD Circuits," Proc. of 2012 IEEE IMS, Montréal, QC, Canada, 17-22 June 2012, pp. 1-3

B. Ravelo & J. Ben Hadj Slama, "Equalization of Digital/Mixed-Signal Disturbances with an Negative Group Delay Circuit," Proc. of 16th IEEE MELECON 2012, Tunisia, 25-28 Mar. 2012, pp. 844-847

B. Ravelo, "Recovery of Microwave-Digital Signal Integrity with NGD Circuits," Photonics and Optoelectronics (P&O), Vol. 2, No. 1, Jan. 2013, pp. 8-16

C/ Principle of NGD equalization

- ❑ To obtain the equalization, we need to generate an output like the input
- ❑ It means that we can assume: $v_{out}(t) \approx v_{in}(t) \rightarrow V_{out}(s) \approx V_{in}(s) \rightarrow V_{out}(s)/V_{in}(s) \approx 1$
- ❑ As analytical solution, you need a function $T(s)$ which verify: $T_p(s) \times T(s) = 1$
- ❑ The unique solution is a LP-NGD function



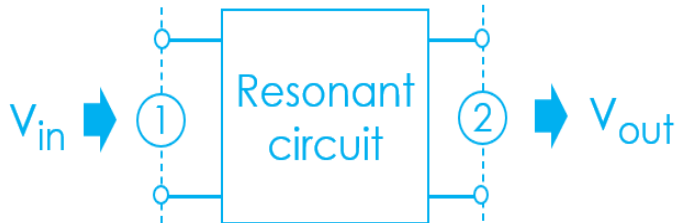
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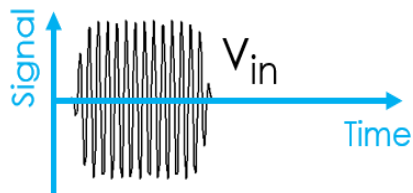
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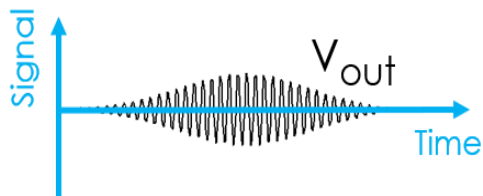
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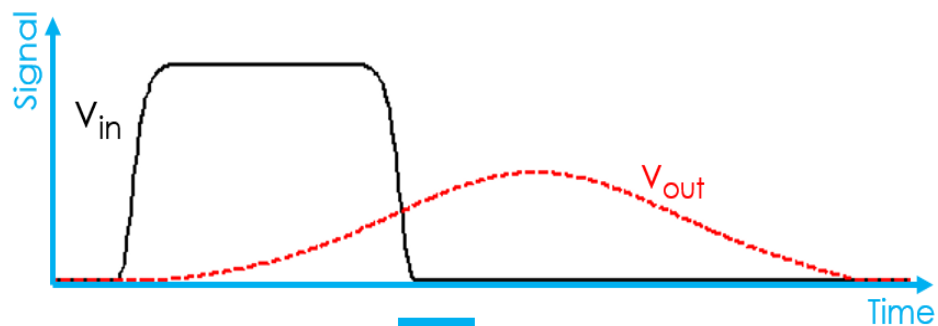
(a)



(b)



(c)



(d)

C/ Principle of NGD equalization

- S-parameter (SP) Laplace symbolic model with reference impedance $R_0=50 \Omega$:

$$[S_r(s)] = [S_{11}(s) \ S_{12}(s); S_{21}(s) \ S_{22}(s)]$$

- For the time-domain analysis, we can assume the TF model which can be updated if we want to consider S_{11} :

$$TF(s) = S_{21}(s) = V_{out}(s) / V_{in}(s)$$

- And the GD model:

$$GD(f) = -\partial \arg[TF(jf)] / (2\pi \partial f)$$

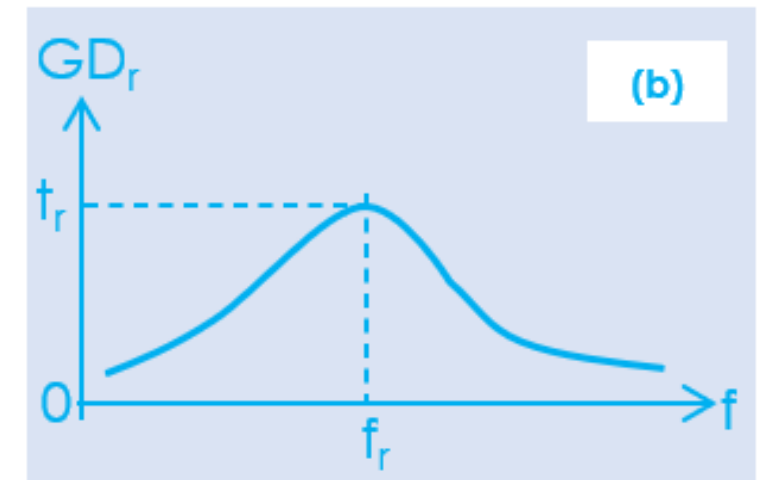
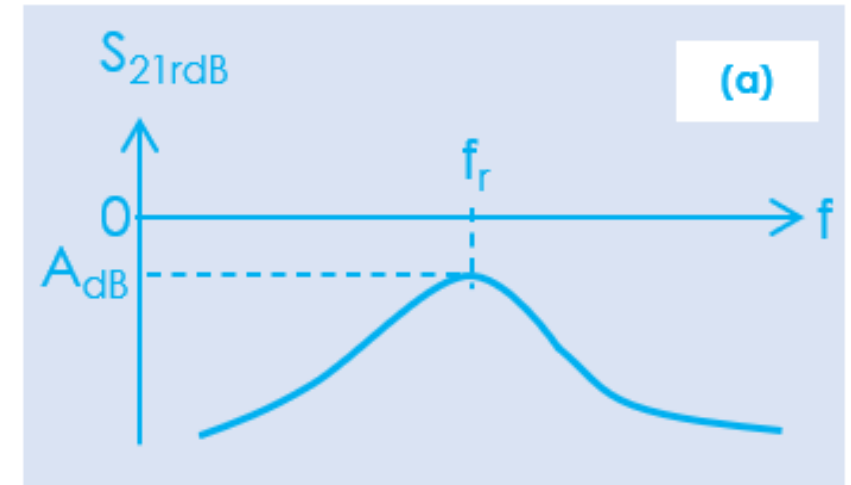
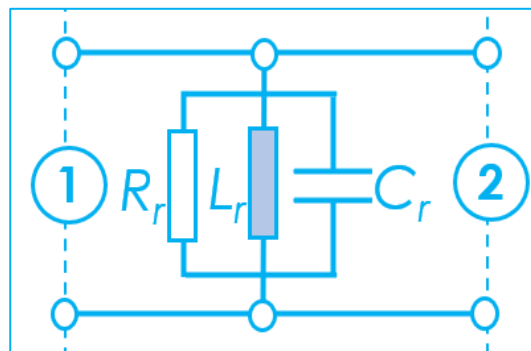
- Due to EMC/EMI resonance \rightarrow The signal integrity (SI) highlighted by transient response v_{out} can be degraded compared to v_{in}
- We are looking for an analytic and design solution to deal on it

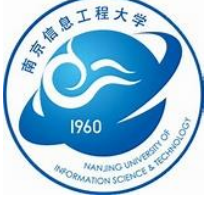
C/ Principle of NGD equalization

- ❑ In the frequency domain, the magnitude behavior can be characterized by $A_{dB} = S_{21rdB}(f_r)$
- ❑ ... Similarity with the GD behavior characterized by $t_r = GD_r(f_r)$
- ❑ Such a behavior can be modelled by $R_r L_r C_r$ tank network characterized by:
 - ✓ Optimal frequency: $f_r = 1/[2\pi\sqrt{L_r C_r}]$
 - ✓ Peak: $A = 2R_r/(R_0 + 2R_r)$
 - ✓ GD: $t_r = 2R_0 R_r C_r / (R_0 + 2R_r) > 0$

❑ The following synthesis equations can be demonstrated

- ✓ $R_r = R_0 A / [2(1-A)]$
- ✓ $C_r = (0.5/R_0 + 1/R_r) t_r$
- ✓ $L_r = 1 / (4\pi^2 f_r^2 C_r)$





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D/ Discussion on PoC result showing resonance reduction

❑ The basic concept of NGD equalization is to find an suitable circuit able to reduce the degradation

❑ Analytical solution:

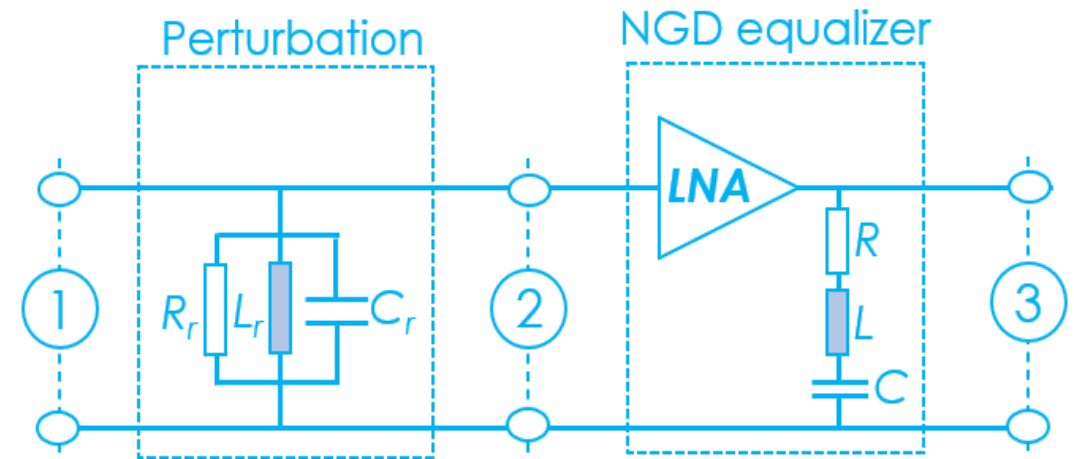
$$\checkmark S_{21r}(s) \times S_{21n}(s) \approx 1 \rightarrow S_{21n}(s) \approx 1/S_{21r}(s)$$

❑ As we have $|S_{21r}(jf_r)| < 1$ and $GD_r(f_r) > 0$, the systemic solution should be:

$$\checkmark \text{ Magnitude: } |S_{21n}(jf_r)| \approx 1/|S_{21r}(jf_r)| > 1$$

$$\checkmark \text{ GD: } GD_n(f_r) \approx -GD_r(f_r) < 0$$

✓ → NGD active circuit (LNA+RLC series network) ☺



B. Ravelo, A. Perennec & M. Le Roy, "Study and Application of Microwave Active Circuits with Negative Group Delay", *Microwave and Millimeter Wave Technologies Modern UWB antennas and equipment*, Chap. 21, Intech Book, Mar. 2010, pp. 415- 439

B. Ravelo, "Recovery of Microwave-Digital Signal Integrity with NGD Circuits", *Photonics and Optoelectronics (P&O)*, Vol. 2, No. 1, Jan. 2013, pp. 8-16

□ The NGD design equations are established from system:

✓ NGD center frequency:

$f_n = 1/[2\pi\sqrt{(L_n C_n)}]$ by solving the equation $f_n = f_r$

✓ Magnitude @ $f_n = f_r$: $|S_{21n}(jf_n)| \approx 1/A$

✓ Or also by considering the access matching (for example $r < -10$ dB) @

$f_n = f_r$: $|S_{11n}(jf_n)| \approx r$

✓ GD value: $GD(f_n) = -t_r$

□ Therefore, we have the following design formulas:

✓ $R = 0.5(1/r - 1)R_0$

✓ $L = 0.25(1 - r)R_0 t_r / r^2$

✓ $C = r^2 / [\pi^2 f_r^2 R_0 t_r (1 - r)]$

✓ LNA gain $G = 1 / (A(1 - r))$

□ From the opposite GD: $GD_n(f_r) \approx -GD_r(f_r) < 0$
 → NGD circuit 😊

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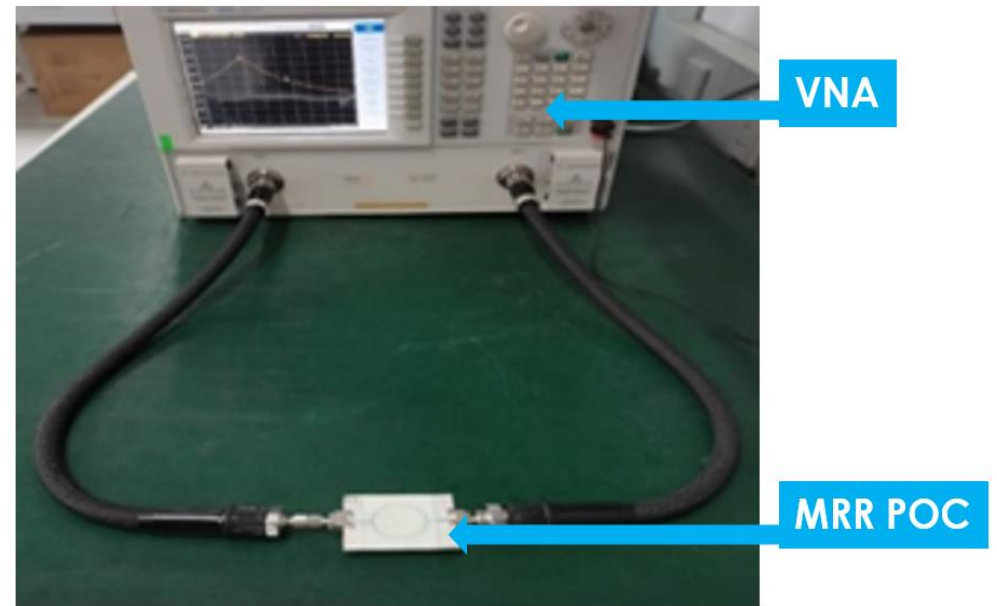
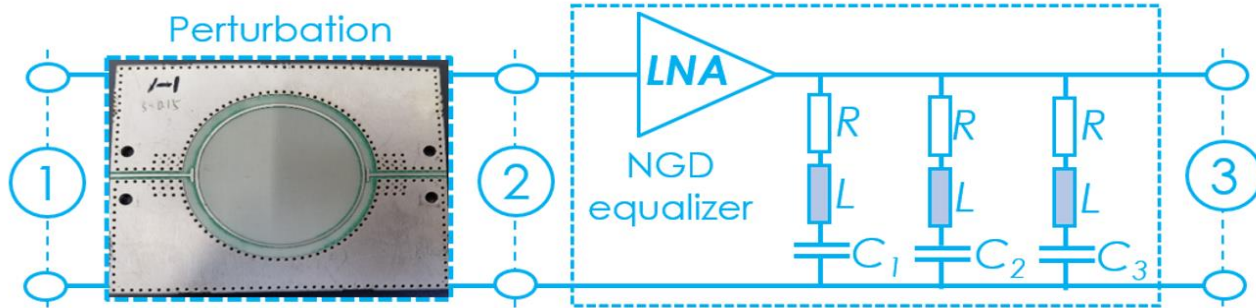
D/ Discussion on PoC result showing resonance reduction

- Design rule and different steps to implement an BP-NGD equalizer:
 - ⇒ *Step 1: Definition of the dispersion effect (center frequency, bandwidth, peak of magnitude)*
 - ⇒ *Step 2: Resonance equivalent circuit modelling*
 - ⇒ *Step 3: BP-NGD topology identification*
 - ⇒ *Step 4: BP-NGD equalizer synthesis*
 - ⇒ *Step 5: POC with simulations*
 - ⇒ *Step 6: Prototyping and fabrication*
 - ⇒ *Step 7: Test and characterization*

- For the present work, we propose a POC with microstrip ring resonator (MRR) to be equalized with NGD active network composed by R, L and C lumped components

D/ Discussion on PoC result showing resonance reduction

- ❑ The POC is a MRR passive circuit constituted by a ring coupled to the access TL and the $R_rL_rC_r$ equivalent model was determined from measured S-parameters
- ❑ 3 cells of NGD circuits constituted by RLC_1 , RLC_2 and RLC_3 parallel network were synthesized from the established design formulas
- ❑ The validation of resonance reduction was performed by SP simulation with ADS® commercial tool from Keysight Technologies®



D/ Discussion on PoC result showing resonance reduction

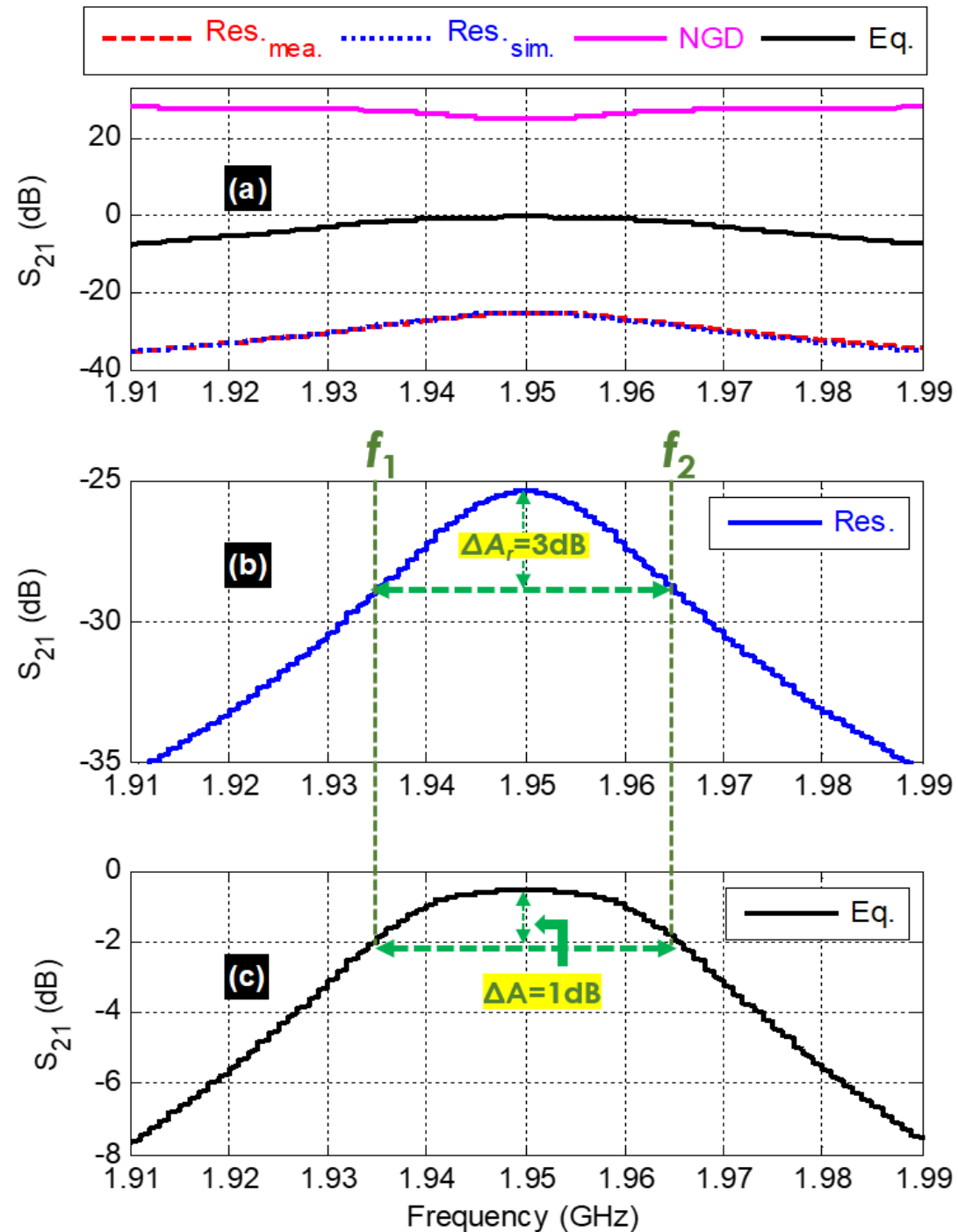
- ❑ The MRR is modelled by $R_r L_r C_r$ corresponding resonance frequency, attenuation and delay indicated by the blue table
- ❑ The NGD circuit parameters as LNA gain, R , L and $C_{k=1,2,3}$ indicated by the green table were calculated from the synthesis formulas by optimizing the equalization effect

Constituting element	Parameter	Value
MRR physical size	Length×Width	57.34×46.2 mm
Substrate relative permittivity	ϵ_r	3.78
Conductor	Length	5 cm
	Width	0.56 mm
Ring resonator	Radius	14 mm
	Gap with access lines	0.1 mm
Resonator measured parameter	f_r	1.95 GHz
	A	-25.36 dB
	t_r	11.9 ns

Role	Component	Name	Value
Equivalent circuit	Resistor	R_r	1.43 Ω
	Inductor	L_r	1.5 pH
	Capacitor	C_r	4.43 nF
NGD	Resistor	R	149 Ω
	Inductor	L	1.77 μ H
	Capacitor	C_1	3.75 fF
LNA	Gain	C_2	3.77 fF
		C_3	3.74 fF
		G	27.9 dB

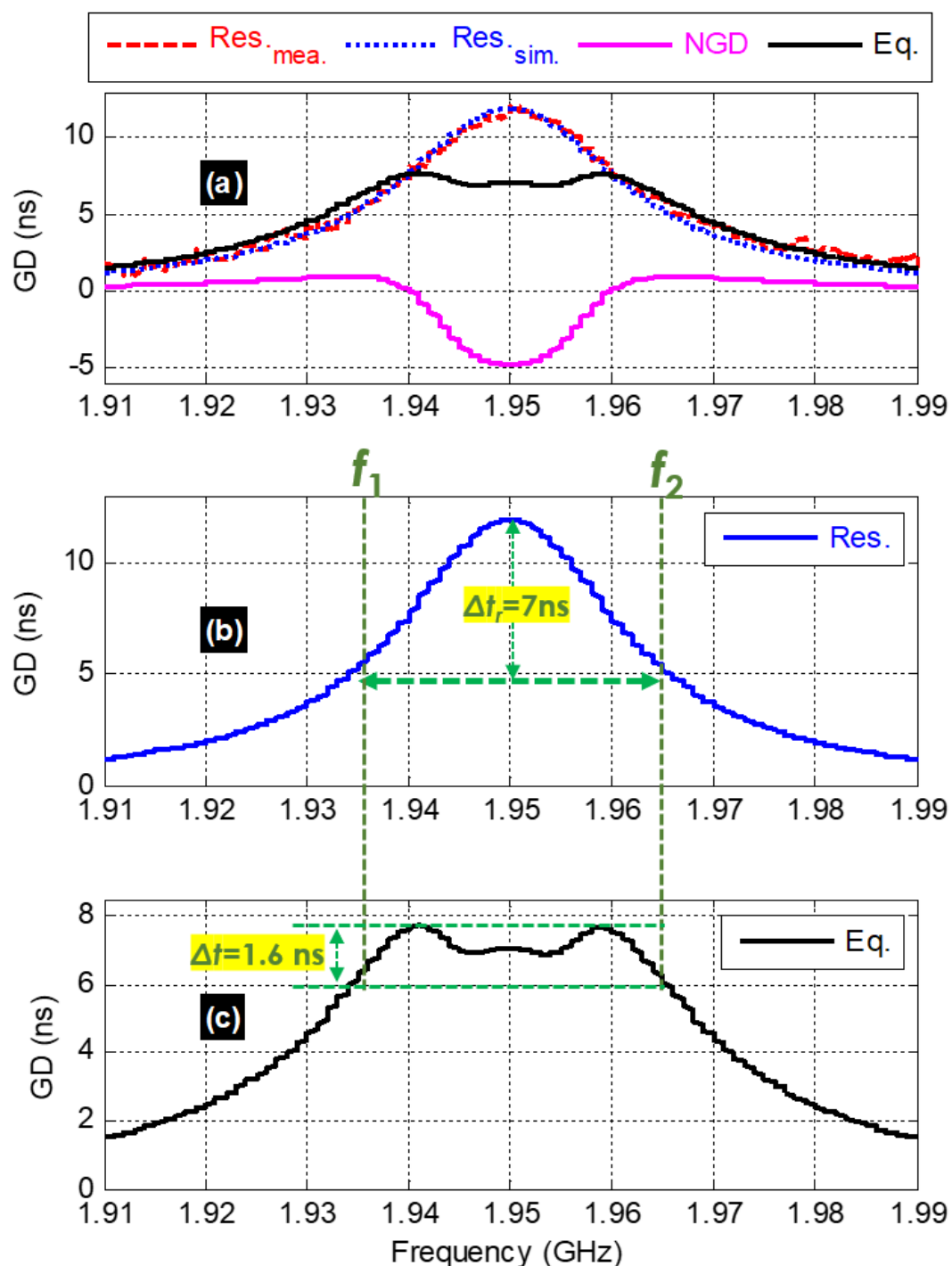
D/ Discussion on PoC result showing resonance reduction

- SP simulation from $f_{\min}=1.91$ GHz to $f_{\max}=1.99$ GHz was proposed
- The frequency domain validation of the NGD equalization method is illustrated by the transmission coeff. magnitudes ($S_{21\text{Res.}}$, $S_{21\text{NGD}}$, $S_{21\text{Eq.}}$)
- Thanks to the NGD-equalization, the transmission coefficient flatness in 3-dB bandwidth $[f_1, f_2]$ with $f_1=1.937$ GHz and $f_2=1.965$ GHz is literally improved



POC	S_{21}	Value
MRR	$\max[S_{21r}(f_r)]$	-25.36 dB
	ΔS_{21r}	3 dB
NGD-MRR	$\max[S_{21}(f_r)]$	-0.5 dB
	ΔS_{21}	1 dB

D/ Discussion on PoC result showing resonance reduction

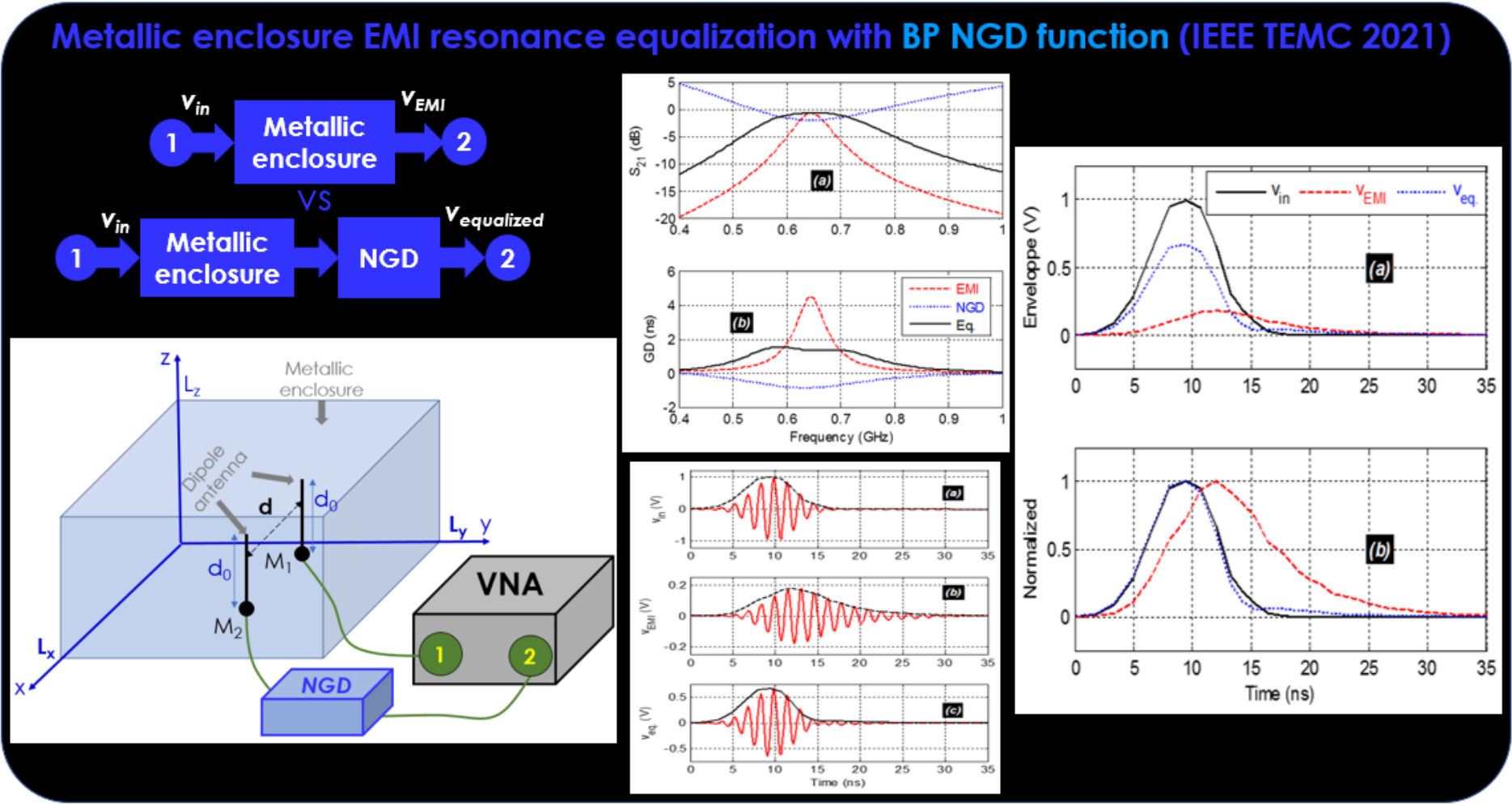


- The resonance effect NGD-equalization feasibility is confirmed by GD response from SP-simulation
- The measured and modelled MRR GDs are in very good correlation
- The GD comparison from resonator, NGD and combined both circuits underlines the flatness improvement notably within the resonator 3-dB bandwidth $[f_1, f_2]$




POC	GD flatness	Value
MRR	Δt_r	7 ns
NGD-MRR	Δt	1.6 ns

D/ Discussion on PoC result showing resonance reduction

B. Ravelo, S. Lalléchère, W. Rahajandraibe, and F. Wan, "Electromagnetic Cavity Resonance Equalization with Bandpass Negative Group Delay," *IEEE TEMC*, Vol. 63, No. 4, Aug. 2021, pp. 1248-1257



E/ Conclusion

-  The SoA on design and experimentation of unfamiliar NGD circuits is overviewed. The BP-NGD theory and design method are presented. The NGD application in EMC/SI engineering for resonant circuit dispersion reduction principle is described.
-  An innovative feasibility study of microstrip structure resonance equalization with BP-NGD circuit is developed. The BP-NGD parameter formulation in function of resonance frequency, transmission coefficient peak and GD is introduced. The validity of the NGD-equalization method is verified with a POC of MRR passive circuit. The equalization result is confirmed with frequency responses of S_{21} and GD flatness.
-  As future work about the NGD-equalization, we are working on the development of IC NGD equalizer to be integrated in the PCBs victim of resonance effect. Our research group is currently developing 180-nm CMOS BP-NGD circuit to fabricate an IC-NGD prototype fulfilling the expected performance of resonance reduction.



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Thank you for your kind
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Questions / comments
please

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